



# COLUMBIA RIVER TEMPERATURE TOTAL MAXIMUM DAILY LOAD

## TECHNICAL ANALYSIS

# Why Develop a Model?

- To determine important processes that affect river temperature
- To quantify the relative impact of different human activities on river temperature
- To run “what-if” scenarios

# Goals of Model Development

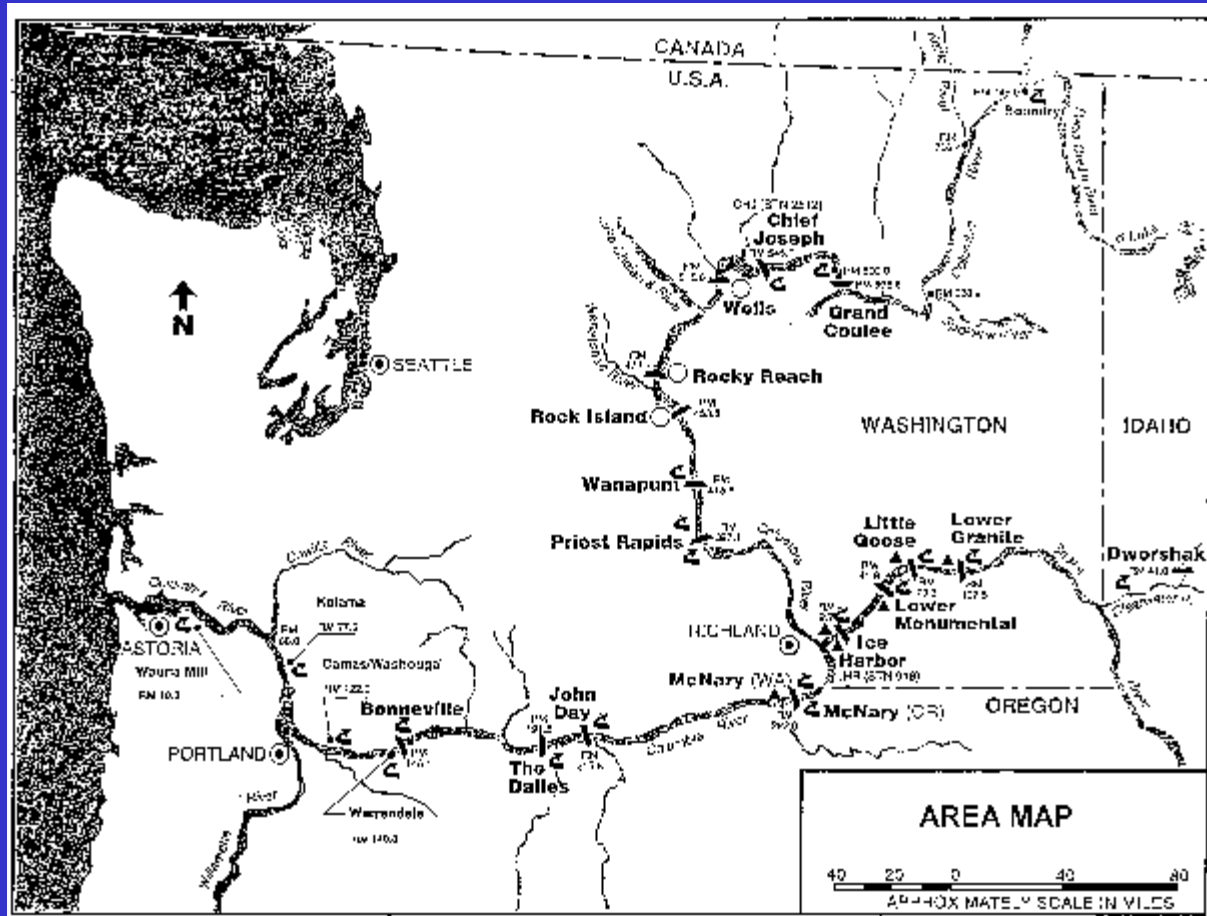
- **Develop a temperature model that:**
  - accurately simulates river temperatures
  - supports a TMDL analysis
- **Keep it non-proprietary, computationally simple and flexible**
- **Conduct Peer Review**
- **Build interface and guide for other users**

## Model Name

- **River**
  - **Basin**
  - **Model developed in EPA Region**
  - **10**
- 
- **RBM10 is written in Fortran code and can be adapted to simulate any large scale river**

COLUMBIA RIVER

# Scale of Analysis - Regional



# **Geographic Boundaries of Model**

- **COLUMBIA RIVER** from International border to Bonneville Dam
  - extension to Astoria in progress
- **SNAKE RIVER** from Brownlee Dam to confluence with Columbia
- **CLEARWATER RIVER** from Orofino to confluence with Snake

# BACKGROUND CONSIDERATIONS



# Water Quality Standards

- **Oregon and Washington Standards for Temperature require evaluation of natural conditions**
  - **Need to estimate temperatures in both impounded and un-impounded conditions**

# System Features

- **Run-of-River Reservoirs**
  - **Vertical temperature stratification relatively low**
  - **Water surface elevation is relatively constant**
    - **points to potential utility of 1-D model with constant impoundment elevation**
    - **previous 1-D studies of Columbia River**

# Available Data

- On the one hand...

- Long term records are available for meteorology, tributary flow, and water temperature, enabling:
  - long term simulations
  - evaluation of system variability, and
  - comparison of simulations to monitored temps

# Data Limitations

- On the other hand...
  - Mainstem Temperature Monitoring
    - Monitoring at Dams Not Designed for Assessment of River Temperature
    - Limited Quality Control/Quality Assurance
  - Tributary Temperature Monitoring
    - Discontinuous Record
    - Unknown Quality Control/Quality Assurance
  - Meteorology
    - Limited Geographical Coverage

# HOW TO ESTIMATE RIVER TEMPERATURE?

# Two Ways to Estimate Temperatures

- **River Temperature Measurements  
(Measurement Model)**
  - Long term scroll case readings at dams
  - Scarce data from unimpounded river
- **Energy Budget  
(Process Model)**

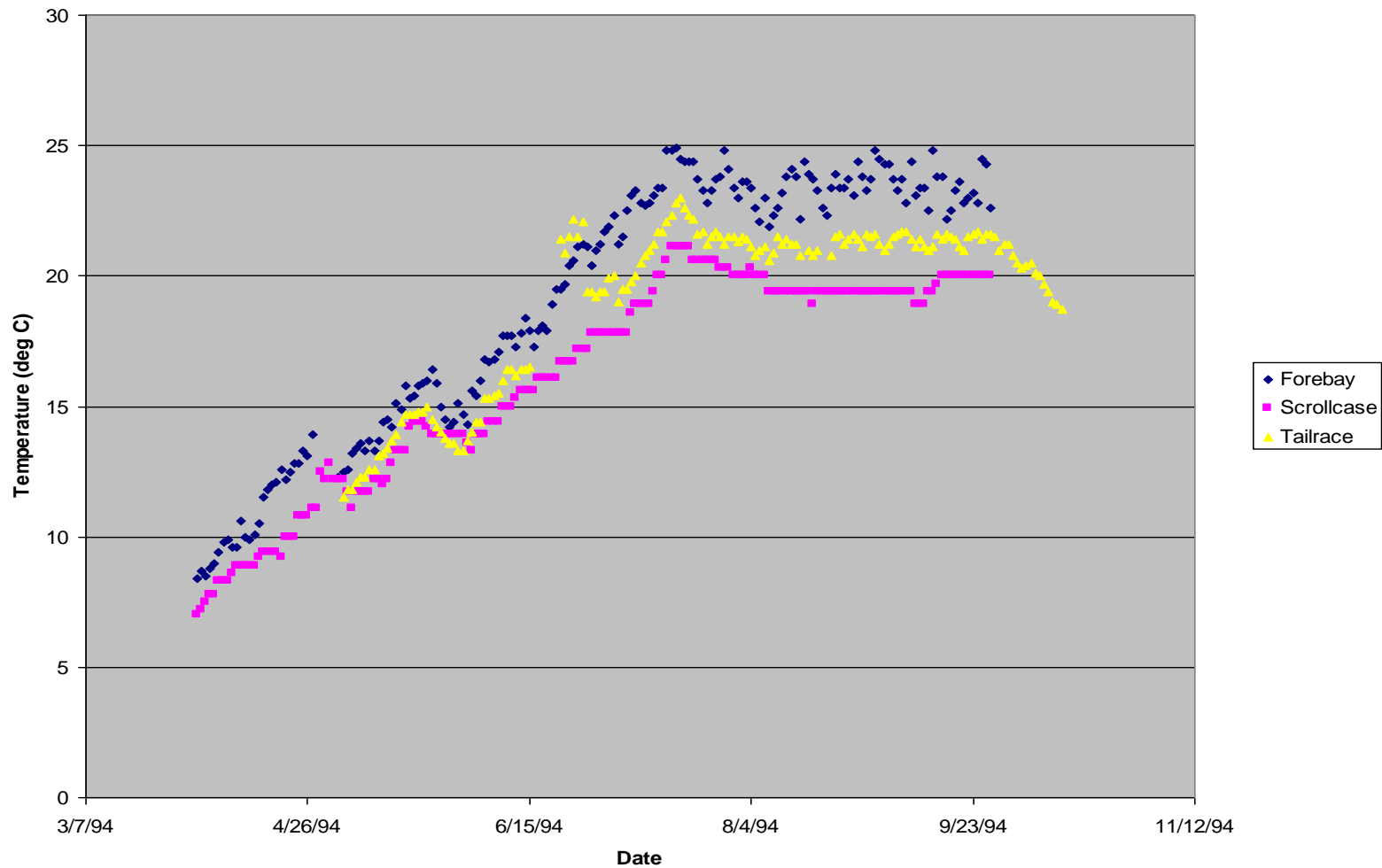
# MEASUREMENT MODEL

# Concept for Measurement Model

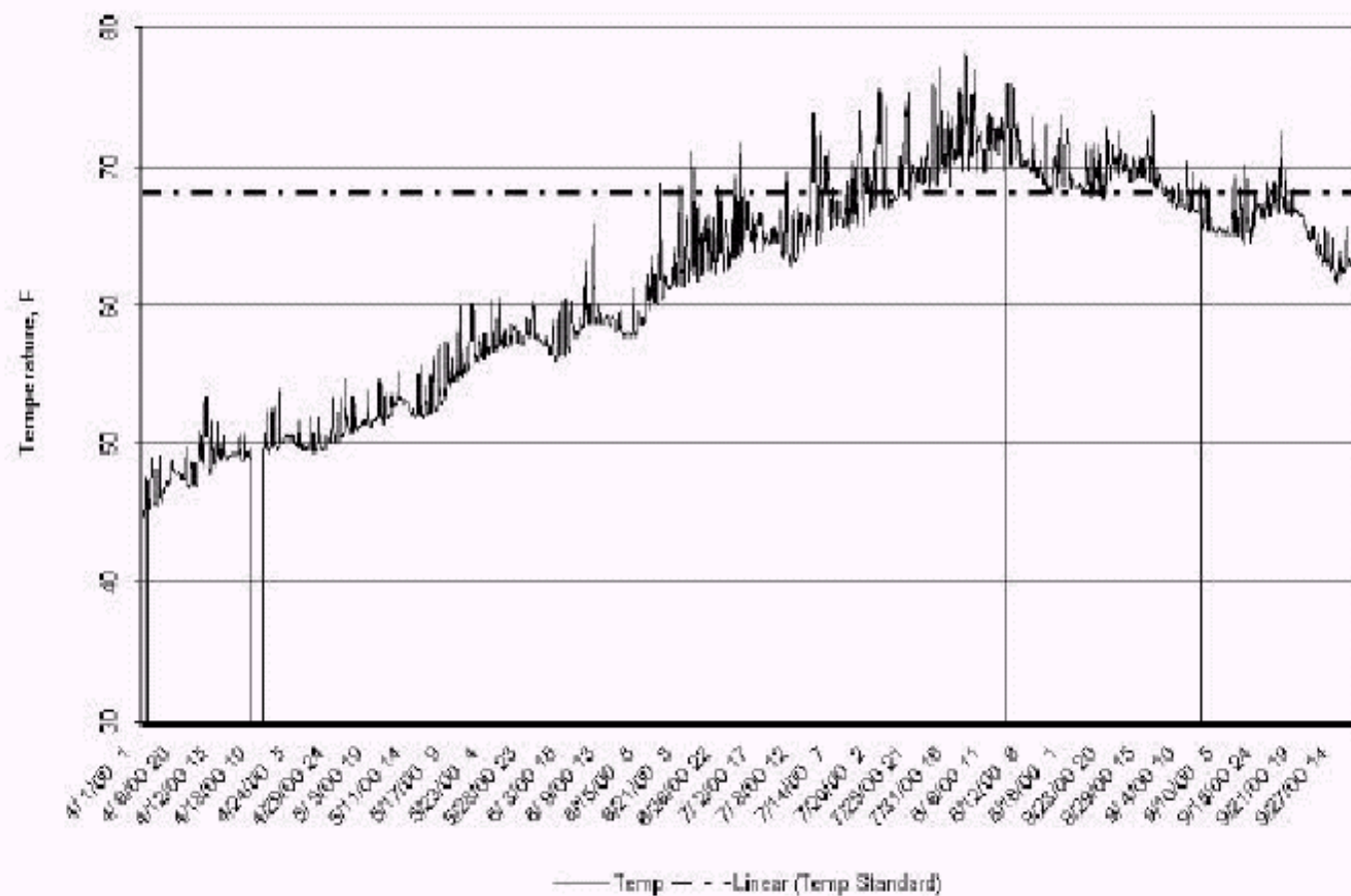
- **Cross-sectionally averaged river temperatures can be estimated based upon:**
  - **Temperature Measurements at Dams (Scroll Case, Forebay, and/or Tailrace)**



Comparison of Daily Water Temperatures at the Scroll Case, Forebay and Tailrace of Ice Harbor Dam,  
1994



# McNary Forebay Oregon Temperature 1 Apr - 30 Sep, 2000



# MEASUREMENT MODEL

$$T_{\text{Actual}} = T_{\text{Observed}} + v$$

TRUE STATE OF  
TEMPERATURE    TEMPERATURE  
MEASUREMENT    MEASUREMENT    MEASUREMENT  
ERROR

# PROCESS MODEL

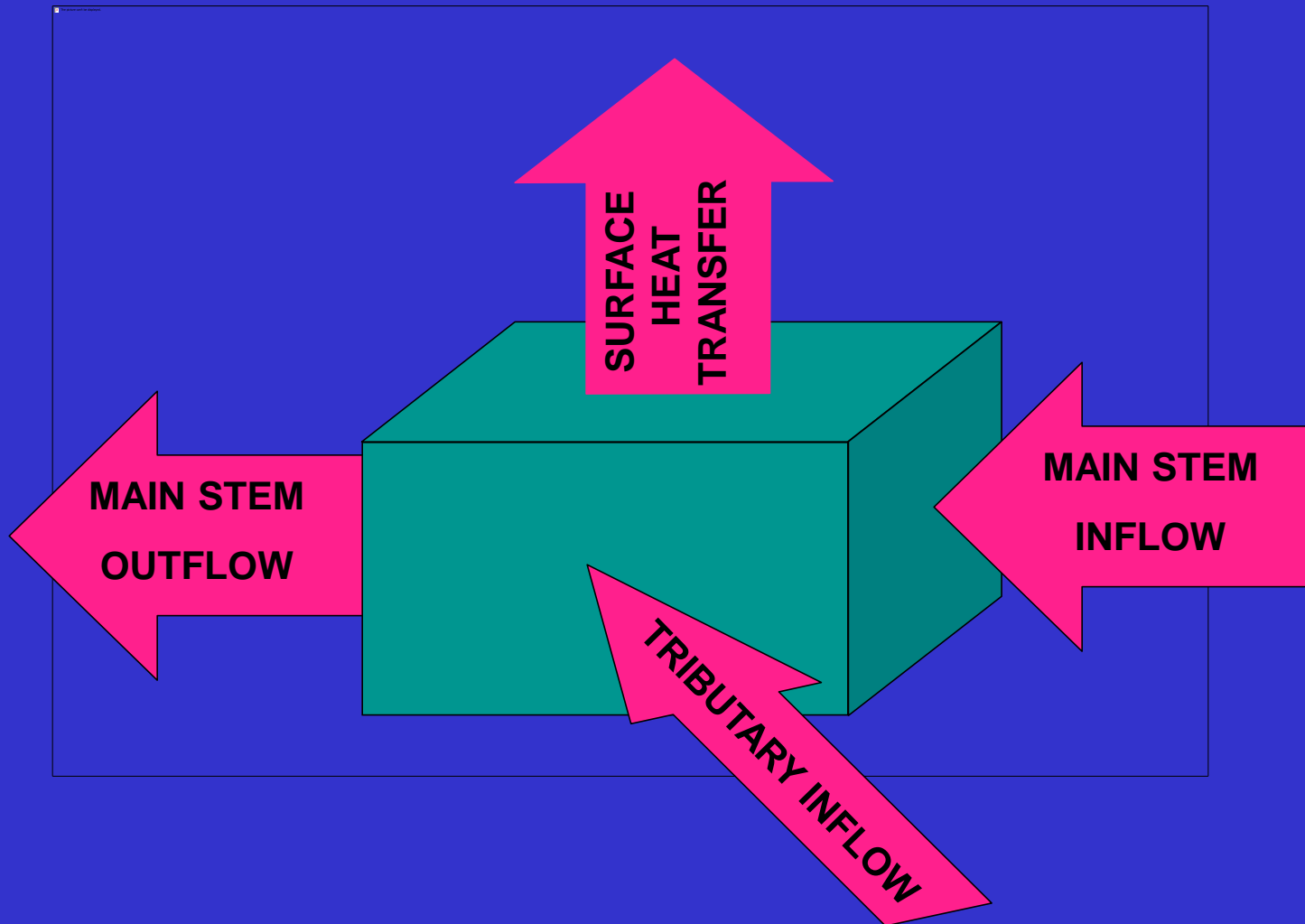
# Why Do We Need Process Model?

- **We need to estimate temperatures under un-impounded conditions for which measurement data is scarce**
- **We have conflicting measurements**
- **We do not have measurements at all river locations of interest**
- **We need to estimate influence of different sources**

# Concept for Process Model

- **Cross-sectionally averaged river temperatures can be estimated based upon:**
  - river flow and geometry
  - surface heat exchange, and
  - advected river and point source heat

# ONE-DIMENSIONAL ENERGY BUDGET MODEL



CHERRYBERRIES  
BERRYANNAZANNE

IN FOOT  
A in

BAKE INEDV OEDV  
NERRY NERRY NERRY

OUT + def +  
B B IC  
P

THIRY SEVENN N  
NRY EXAKE NRY



# INFORMATION NEEDS

## **General**

- **System Topology**
- **Latitude of Site**
- **Day of the Year**

## **River Geometry - Existing and Unimpounded**

- **Cross-sectional Area**
- **Width of River**
- **River Mile**

## **Main Stem**

- **Main Stem Boundary Inflows**
- **Main Stem Boundary Temperatures**

## **Tributary**

- **Tributary and Point Source Flows**
- **Tributary and Point Source Temperatures**

# **Meteorology**

- **Cloud Cover**
- **Dry Bulb Temperature**
- **Wind Speed**
- **Vapor Pressure of the Air near the Water Surface**
- **Atmospheric Pressure**

# AVAILABLE INFORMATION

<i>Type of Data</i>	<i>EPA's Available Information in Study Area</i>
<i>Tributary Temperature</i>	19 Stations 30 Year Record - Discontinuous - Grab Samples
<i>Mainstem Temperatures</i>	Scroll Case, Tailrace, Forebay of USACE Dams 30 Year Record – Discontinuous – Daily Obs.
<i>River Geometry</i>	Existing Conditions: Approx. 100 profiles Natural Conditions: Approx. 150 profiles
<i>Flow</i>	22 USGS Gages 30 Year Record – Continuous – Daily Observations
<i>Meteorology</i>	3 First Order Stations, 2 Local Air Temp Stations 30 Year Record – Continuous – Hourly Observations

# Data Retrieval & Formatting Challenge

- **Data Cornucopia**
  - large scale, many monitoring locations
  - voluminous data
  - numerous formats, sample types, etc.
  - data gaps
  - outliers
- **Making Data Usable for RBM10**
  - adhoc utilities for formatting and calculating necessary input data

# IMPORTANT ASSUMPTIONS



# Important Assumptions

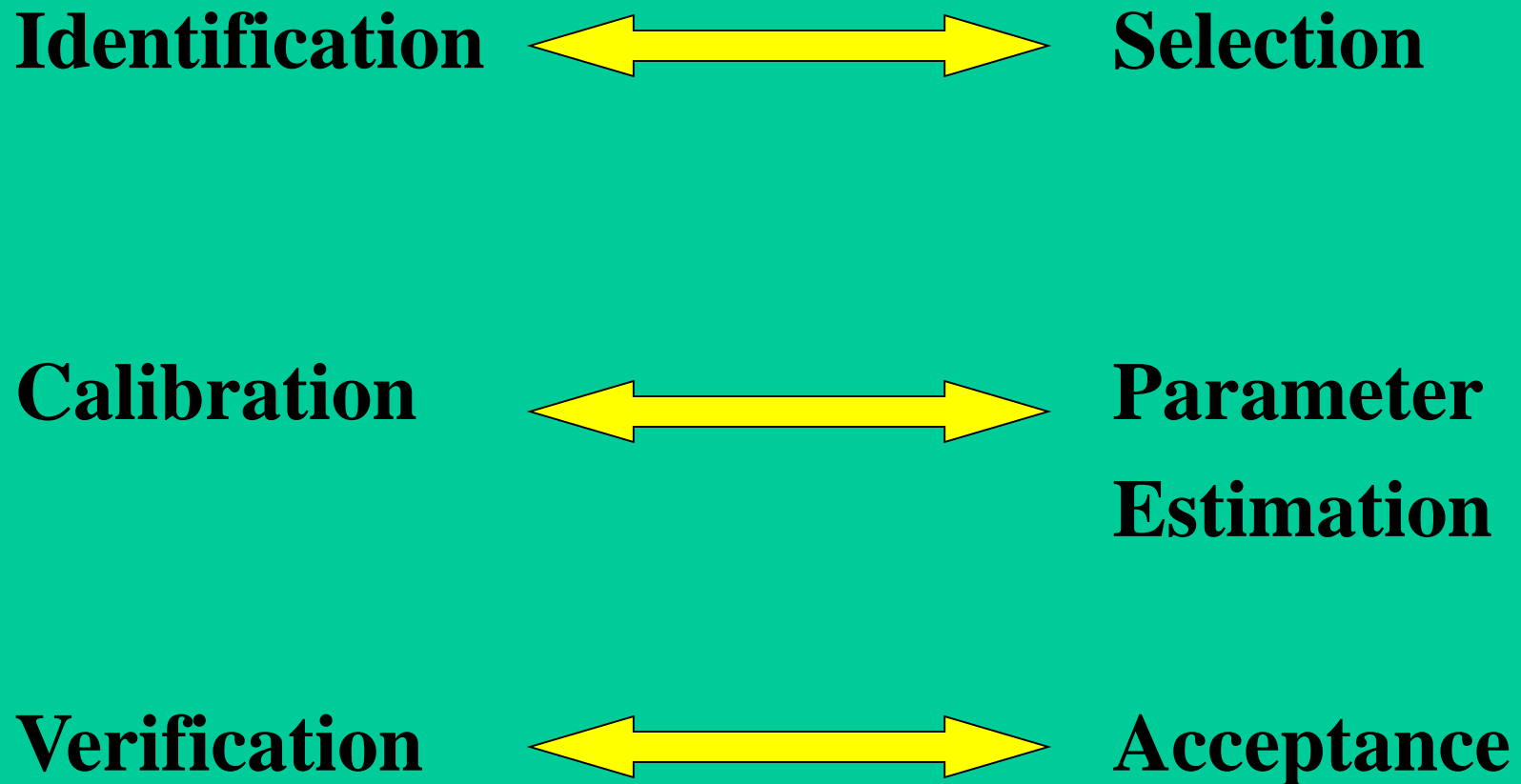
- **Meteorology**
  - Described by five regional weather stations
- **Mainstem Flow**
  - Constant elevation for impounded reaches except Grand Coulee
  - Leopold relations developed from gradually-varied flow methods for un-impounded reaches
- **Tributary Temperatures**
  - Mohseni relations developed from local air temperature and weekly/monthly river monitoring

# Important Assumptions

- **Groundwater**
  - Hyporheic flow does not significantly change the cross-sectionally averaged temperature in unimpounded conditions
- **Measurement Model**
  - Tailrace monitoring represents best available measure of cross-sectionally averaged temperatures

# MODEL DEVELOPMENT

# TERMINOLOGY



# MODEL SELECTION

- **1-Dimensional, Time Dependent**
- **Estimates of Water Temperature from Process and Measurement Models Treated as Random Variables**
- **Mixed Lagrangian-Eulerian solution technique  
“Reverse Particle Tracking”**
  - reduces error due to numerical dispersion
  - reduces numerical instability
  - reduces computational burden of uncertainty evaluation

# PARAMETER ESTIMATION

- Identify parameters that govern rates of energy transfer in the system
  - Some are well known (e.g., solar declination)
  - Some are less well known (e.g., evaporation rates)
- Two parameters that are less known are estimated
  - evaporation rates
  - assignment of area covered by 5 meteorological stations

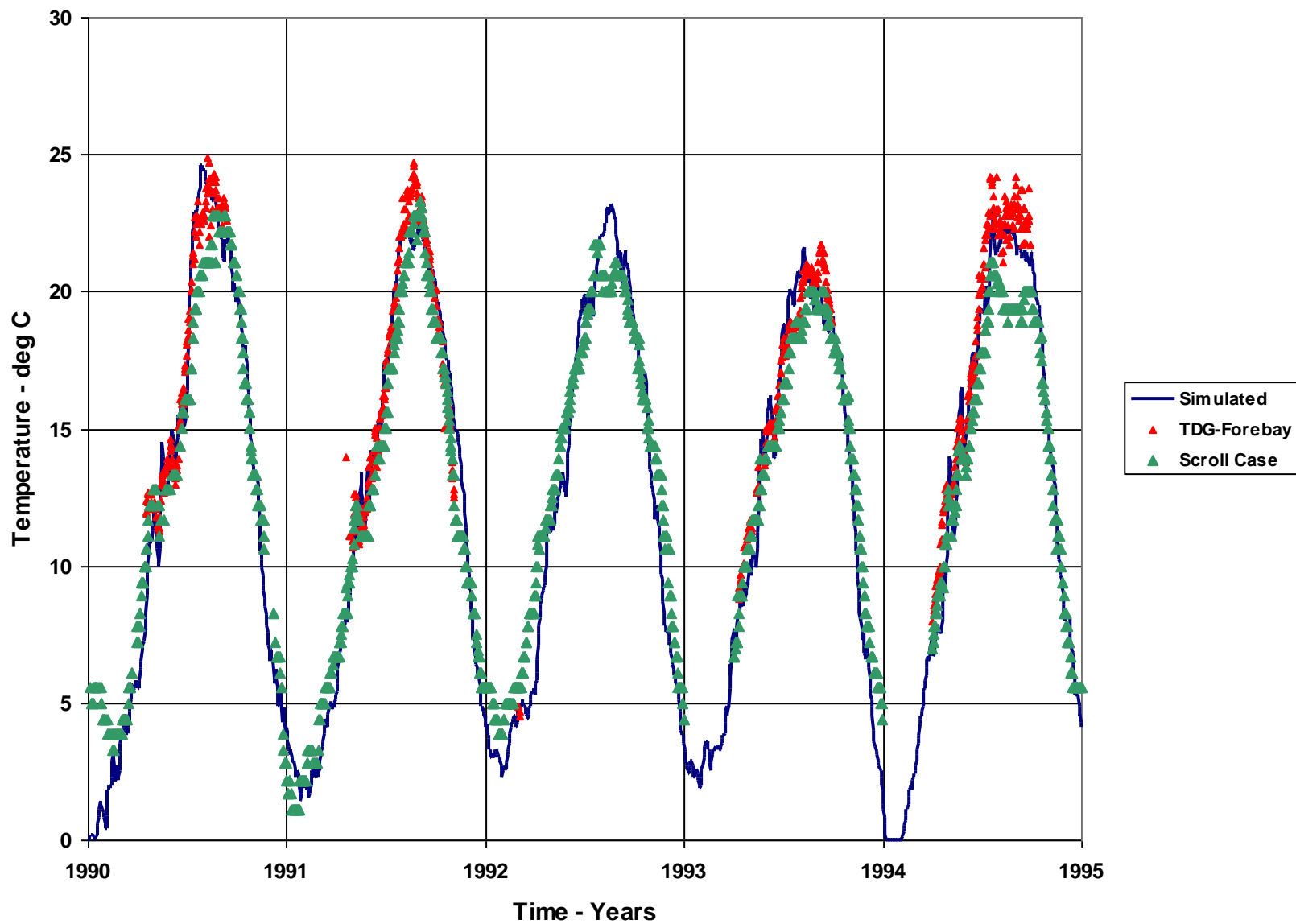
# ACCEPTANCE CRITERIA

- Estimates for evaporation rates and meteorological station assignment are varied to satisfy criteria for model acceptance
- Acceptance criteria:
  - solutions are unbiased; and
  - error is uncorrelated in time

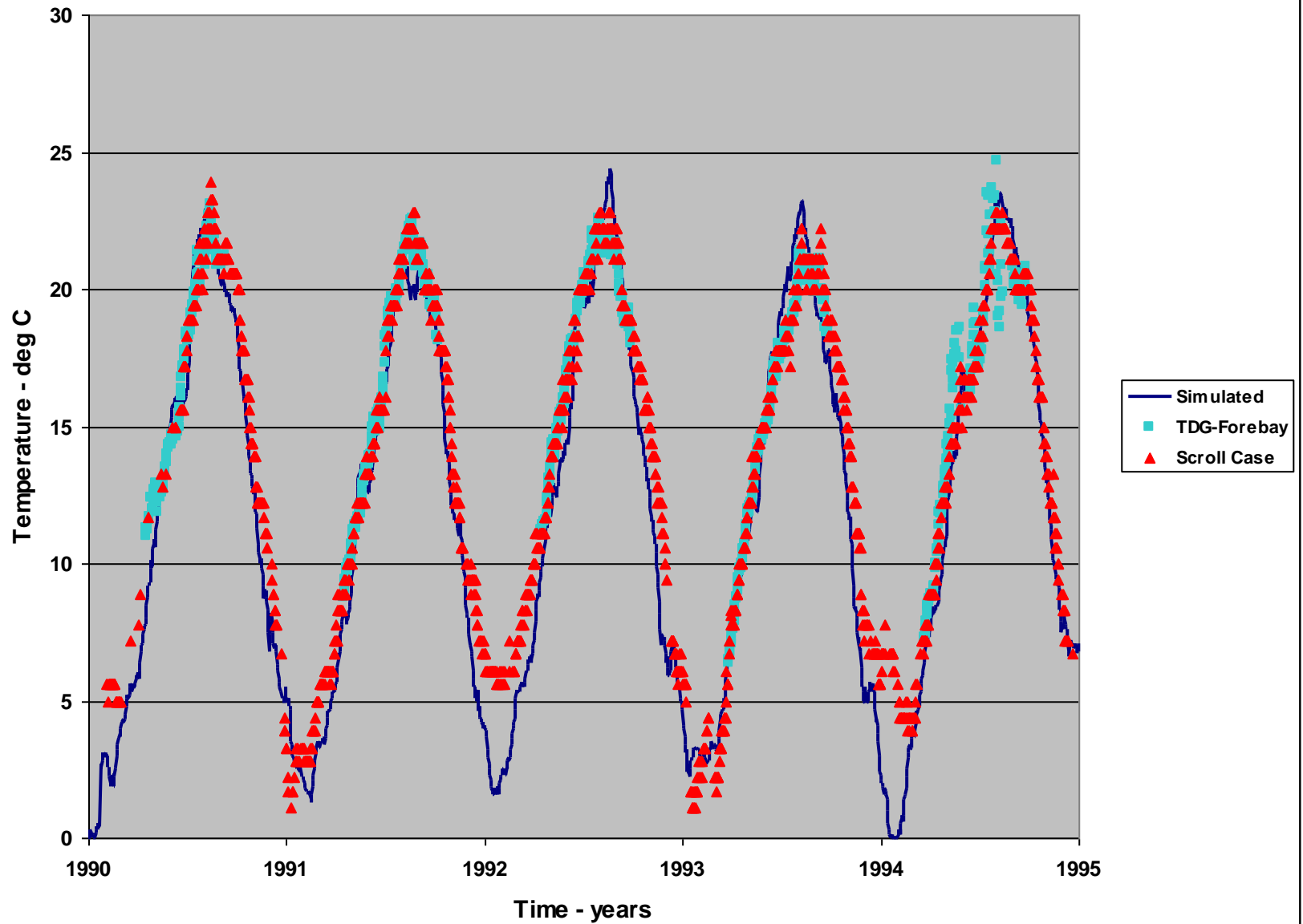
# MODEL APPLICATION AND ACCEPTANCE



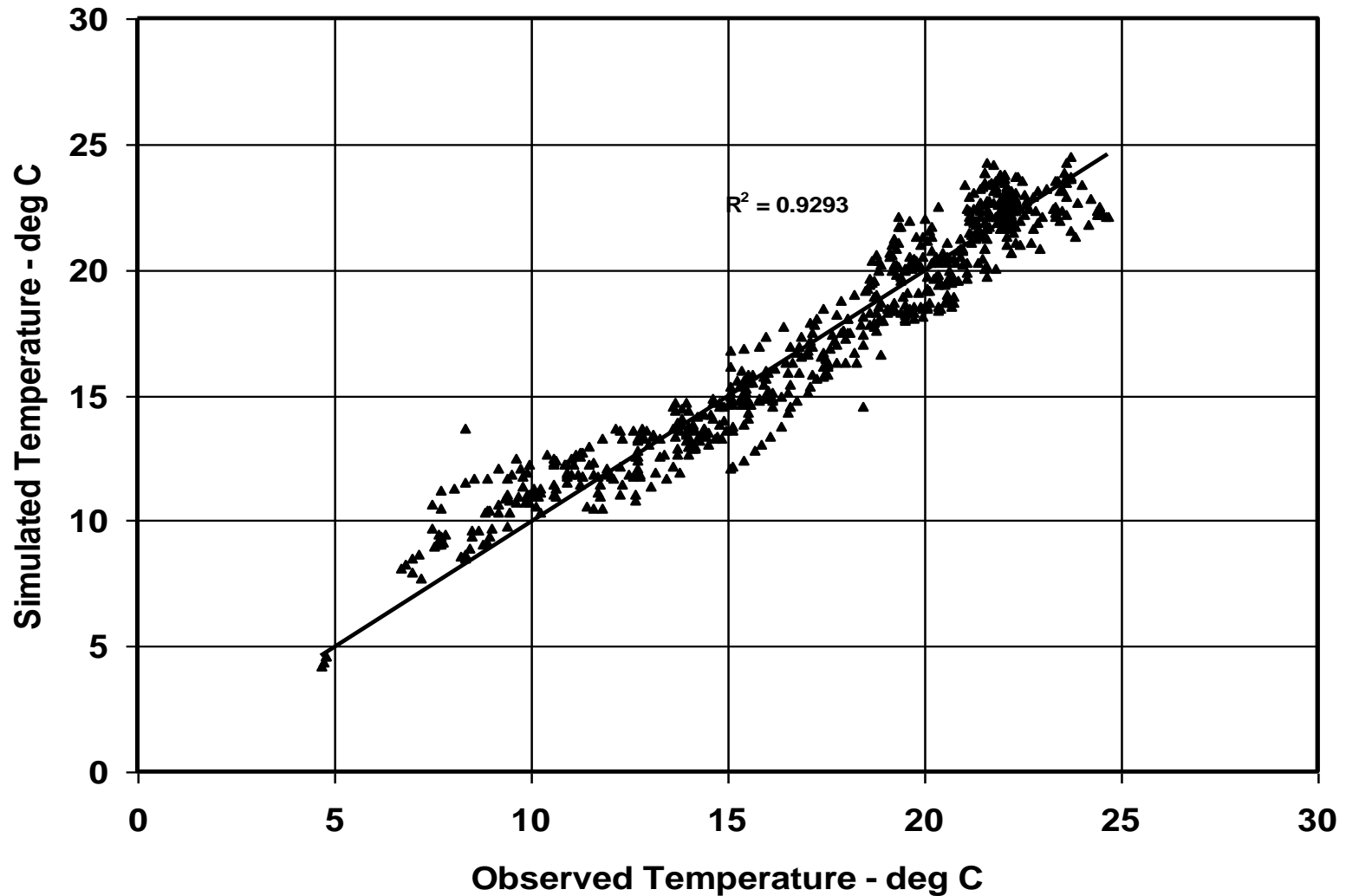
Simulated and Observed Water Temperatures at Ice Harbor



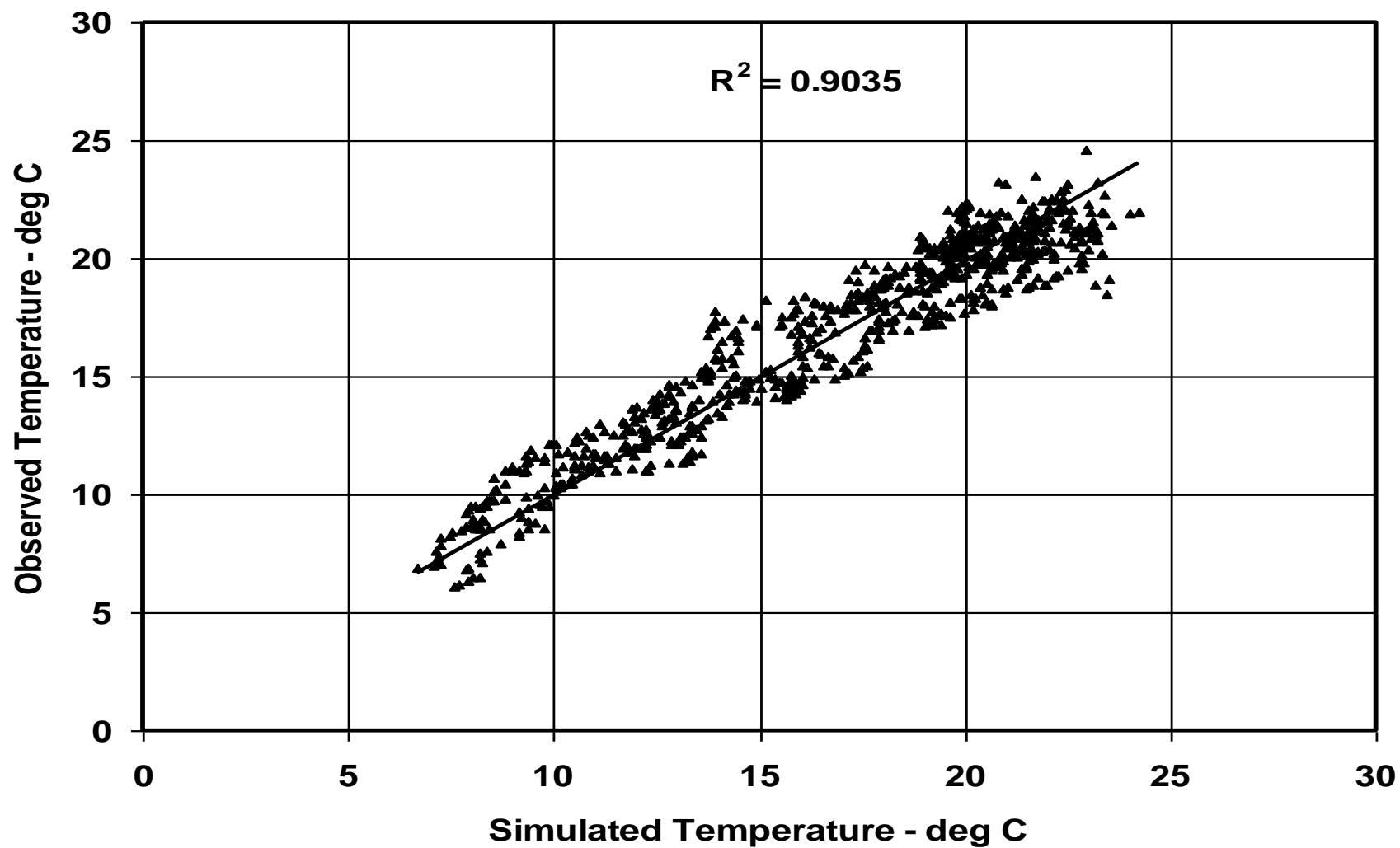
Simulated and Observed at Bonneville Dam



**Figure D-6. Regression of observed on simulated at Ice Harbor  
Dam 1990-1995**



**Figure D-5. Regression of observed on simulated at Bonneville Dam 1990-1995.**



## RBM10 Results for 1990-1994

<b><i>Location</i></b>	<b><i>Mean Difference (Obs-Sim)</i></b>	<b><i>Standard Deviation</i></b>
<b><i>Snake River @Ice Harbor</i></b>	0.05 deg C	1.2
<b><i>Columbia River @Bonneville</i></b>	0.04 deg C	1.3

## Error Estimates from Other Studies

- **RISLEY (1997) - Tualatin River**  
Max Mean Difference = 3 Deg C  
Mostly < 1 Deg C
- **BATTELLE-MASS1 (2001) - Columbia River**  
RMS Error = 0.59 - 1.52 Deg C
- **HDR/PORTLAND STATE/IPC (1999) - Snake River**  
AME = 0.6-2.3 Deg C (1992 data)  
AME = 0.5-2.0 Deg C (1995 data)
- **CHEN (1996) - Grande Ronde River**  
Error = -2.20 - 8.28 Deg C (Summer Max)  
Error = -1.21 - 7.69 Deg C (Avg 7-day Max)